

Efficient Algorithms for Resistance and Capacitance Calculation Problems in the Design of Flat Panel Display

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## Outline

Background of FPD Design Automation

A Hybrid Method for Calculating Wire Resistance
 Floating Random Walk Based Capacitance Solver
 Conclusions

# Background

We are surrounded by FPDs

- □ Very-large, high-brightness displays
- □ Small-area, high-resolution, low-power
- Thin-film transistor (TFT) based active matrix technology
- □ LCD, OLED with glass/plastic substrate
- Designing high-performance/low-cost FPDs
- The CAD flow for FPD Design
  - Wire resistance and capacitance need be calculated to validate the signal timing and high display quality









# Background

The difference to the parasitic extraction of VLSI circuit

- The proximity of interconnect wires is less, so that capacitance is smaller and contributes less to signal delay
- Instead of pursuing small delay, the object in FPD design is keeping almost equal signal delay to display pixels
   Wire resistance calculation is important

### Touch panel technology

- □ Largely enhance the interactivity and user experience
- TP-FPD includes more complex internal structure
- Capacitive touch sensor has advantages in durability, reliability and capability
- Accurate capacitance calculation is needed



# Background

### Our contributions

- □ A resistance calculation technique for FPD wire design
- A capacitance calculation technique for TP design
- They are more efficient than existing techniques, and are applied to actual FPD and TP-FPD designs

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### Structure characteristics

- Narrow routing area and equal-resistance object make wires with very complex geometry
- □ Since planar manufactory technology is employed, the wire geometry can often be regarded as a 2-D structure





#### 2-D boundary element method

- With an automatic boundary partition approach, it works well for some small structures
- For the long-wire structure, a lot of unknowns involved
- An analytical-BEM coupled approach
  - Follows the divide-and-conquer idea
  - Divide the wire into some portions with long rectangle shape and the remaining portions
  - The rectangle part is solved with analytical formula
  - The remain parts are solved with BEM individually
  - □ Their results are combined to get the final result

Algorithm 1: The analytical-BEM coupled approach

 $1: \mathbf{R} := 0;$ 

- 2: Calculate the tilt angle  $\theta_i$ , (*i*=1, ..., *n*) of all outer-loop edges of the wire profile;
- 3: For i=1,...,n //*n* is the number of outer-loop vertices
- 4: **For** j=i+1,...,n
- 5: If  $|\theta_i \theta_i| < \theta_{tol}$ , then
- 6: Calculate the valid rectangle;
- 7: If there is a rectangle with length/width ratio>  $\eta$ , then
- 8: Obtain a long-wire rectangle by cutting length of 3X width from the both ends of the valid rectangle;
- 9: Calculate resistance  $R_{rec}$  of the long-wire rectangle;
- 10:  $R := R + R_{rec};$
- 11: Cut off the long-wire rectangle, and adjust ports;
- 12: **Endif**
- 13: **Endif**
- 14: **Endfor**
- 15:Endfor

16:For each left portion of the wire,

17: Use BEM to calculate resistance  $R_{lef}$ ;

- 18:  $R := R + R_{lef};$
- 19:EndFor

- Numerical results of Res2d
  - Use LAPACK to solve Ax=b in BEM
  - Experiments on a Linux server with Xeon 6-core CPU
  - $\Box$  Several FPD wires are calculated (assuming  $\sigma$ =1)
  - Results compared with Raphael RC2 (golden tool)

|      | Raphael RC2 |                        |        | Res2d    |        |       |      |                  |
|------|-------------|------------------------|--------|----------|--------|-------|------|------------------|
| Case | #orid       | R                      | Time   | #alamont | R      | Error | Time |                  |
|      | #gria       | $(\Omega \cdot \mu m)$ | (s)    | #element | (Ω·µm) | (%)   | (s)  |                  |
| 1    | 703K        | 4.158                  | 2513.4 | 3873     | 4.183  | 0.60  | 5.54 |                  |
| 2    |             |                        |        | 1547     | 261.2  |       | 1.48 | 300X~400X        |
| 3    | 100K        | 91.43                  | 82.3   | 848      | 90.87  | -0.61 | 0.25 | Faster!          |
| 4    | 57K         | 2.092                  | 40.1   | 280      | 2.08   | -0.57 | 0.01 | 1 <i>uster</i> . |
| 5    |             |                        |        | 3931     | 1770   |       | 5.92 |                  |

### Numerical results of Res2d (a real design)



Res2d costs 15.3 seconds to calculate the resistance. The result is 18.138  $\Omega$ , which well matches the result from a third-party solver based on FEM.

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### Structure complexity

- Touch sensor, FPD wires, finger stylus
- Calls for 3-D field-solver solution
- Methods for 3-D capacitance solver
  - Finite difference/finite element method
    - □ Stable, versatile; slow

Boundary element method

- Fast, handle complex geometry
- Not scalable, need discretization (may affect accuracy)

Ax = b

- □ Floating random walk method
  - □ Scalable for large problem (low memory cost)
  - No discretization of problem domain (stable accuracy)





FastCap, Act3D QBEM/HBBEM

QuickCap/Rapid3D, RWCap

The basics of FRW method

Integral formula for the electrostatic potential

$$\phi(\boldsymbol{r}) = \oint_{S_1} P_1(\boldsymbol{r}, \boldsymbol{r}^{(1)}) \phi(\boldsymbol{r}^{(1)}) ds^{(1)}$$

P<sub>1</sub> is called surface Green's function, and can be regarded as a probability density function  $\Box \text{ Monte Carlo method: } \phi(r) = \frac{1}{M} \sum_{m=1}^{M} \phi_m$ 

Transition domain

 $\phi_{m} \text{ is the potential of a point on } S_{1}, \text{ randomly sampled with } P_{1}$   $\square \text{ What if } \phi_{m} \text{ is unknown? expand the integral recursively }$   $\phi(\boldsymbol{r}) = \oint_{S_{1}} P_{1}(\boldsymbol{r}, \boldsymbol{r}^{(1)}) \oint_{S_{2}} P_{1}(\boldsymbol{r}^{(1)}, \boldsymbol{r}^{(2)}) \cdots$   $for a point on S_{1}, \text{ randomly sampled with } P_{1}$   $\phi(\boldsymbol{r}) = \oint_{S_{1}} P_{1}(\boldsymbol{r}, \boldsymbol{r}^{(1)}) \oint_{S_{2}} P_{1}(\boldsymbol{r}^{(1)}, \boldsymbol{r}^{(2)}) \cdots$   $for a point on S_{1}, \text{ randomly sampled with } P_{1}$   $\phi(\boldsymbol{r}) = \oint_{S_{1}} P_{1}(\boldsymbol{r}, \boldsymbol{r}^{(1)}) \oint_{S_{2}} P_{1}(\boldsymbol{r}^{(1)}, \boldsymbol{r}^{(2)}) \cdots$   $for a point on S_{1}, \text{ randomly sampled with } P_{1}$   $\phi(\boldsymbol{r}) = \oint_{S_{1}} P_{1}(\boldsymbol{r}, \boldsymbol{r}^{(1)}) \oint_{S_{2}} P_{1}(\boldsymbol{r}^{(1)}, \boldsymbol{r}^{(2)}) \cdots$   $for a point on S_{1}, \text{ randomly sampled with } P_{1}$   $\phi(\boldsymbol{r}) = \oint_{S_{1}} P_{1}(\boldsymbol{r}, \boldsymbol{r}^{(1)}) \oint_{S_{2}} P_{1}(\boldsymbol{r}^{(1)}, \boldsymbol{r}^{(2)}) \cdots$   $for a point on S_{1}, \text{ randomly sampled with } P_{1}$   $for a point on S_{1}, \text{ randomly sampled with } P_{1}$   $\phi(\boldsymbol{r}) = \oint_{S_{1}} P_{1}(\boldsymbol{r}, \boldsymbol{r}^{(1)}) \oint_{S_{2}} P_{1}(\boldsymbol{r}^{(1)}, \boldsymbol{r}^{(2)}) \cdots$   $for a point of a point on S_{1}, \text{ randomly sampled with } P_{1}$   $for a point of a point on S_{1}, \text{ randomly sampled with } P_{1}$   $\phi(\boldsymbol{r}) = \oint_{S_{1}} P_{1}(\boldsymbol{r}, \boldsymbol{r}^{(1)}) \oint_{S_{2}} P_{1}(\boldsymbol{r}^{(1)}, \boldsymbol{r}^{(2)}) \cdots$   $for a point of a point of a point on S_{1}, \text{ randomly sampled with } P_{1}$   $for a point of a point of a point on S_{1}, \text{ randomly sampled with } P_{1}$   $for a point of a point of a point of a point on S_{1}, \text{ randomly sampled with } P_{1}$  for a point of a poin

- The Markov random process + MC method prove the correctness of the FRW method
- A 2-D example with 3 walks
  Use maximal cubic transition domain
  How to calculate capacitances?
  C<sub>11</sub> C<sub>12</sub> C<sub>13</sub> V<sub>1</sub> Q<sub>1</sub>

Definition:  $\begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{12} & C_{22} & C_{23} \\ C_{13} & C_{23} & C_{33} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \end{bmatrix} = \begin{bmatrix} Q_1 \\ Q_2 \\ Q_3 \end{bmatrix} \longrightarrow Q_1 = C_{11}V_1 + C_{12}V_2 + C_{13}V_3$ 

Integral for calculating charge (Gauss theorem)

$$Q_{1} = \oint_{G_{1}} F(\boldsymbol{r}) \cdot \hat{n} \cdot \nabla \phi(\boldsymbol{r}) d\boldsymbol{r} = \oint_{G_{1}} F(\boldsymbol{r}) \cdot \hat{n} \cdot \nabla \oint_{S_{1}} P_{1}(\boldsymbol{r}, \boldsymbol{r}^{(1)}) \phi(\boldsymbol{r}^{(1)}) ds^{(1)} ds$$
$$= \oint_{G_{1}} F(\boldsymbol{r}) g \oint_{S_{1}} P_{1}(\boldsymbol{r}, \boldsymbol{r}^{(1)}) \phi(\boldsymbol{r}^{(1)}) \omega(\boldsymbol{r}, \boldsymbol{r}^{(1)}) ds^{(1)} ds \qquad \text{weight value, estimate of} \\ C_{11}, C_{12}, C_{13} \text{ coefficients} \end{cases}$$

- The secrets of fast FRW solver for VLSI interconnects
  - Cubic transition domain fits geometry
  - Numerically pre-calculate transition probabilities and weight values
  - Importance sampling; placement of Gaussian surface; space management



### Differences in VLSI design & TP-FPD design

Cap. Extract. for VLSI vs. Cap. Simul. for TP-FPD

| Conductor   | Mostly Manhattan         | Generally non-            |  |  |
|-------------|--------------------------|---------------------------|--|--|
| geometry    | shape, with moderate     | Manhattan shape, with     |  |  |
| geometry    | aspect ratio             | very large aspect ratio   |  |  |
| Dielectric  | On-chip dielectric       | In-device dielectrics and |  |  |
| anvironment | insulators; relatively   | out-device air; arbitrary |  |  |
| environment | fixed dielectric profile | dielectric configuration  |  |  |
| Accuracy    | Mainly self-capacitance  | Need accurate coupling    |  |  |
| demand      | for delay calculation    | capacitances              |  |  |



### Proposed techniques

- Geometry engine for non-Manhattan metal shape, which allows planar rotation of transition cube
- A unified dielectric pre-characterization approach
  - Dielectric homogenization or a new approach?



Works only if the permittivity ratio  $\leq$  2, and Has larger error

Pre-characterize the two-dielectric configurations with  $0.1 \le r < 1$ ; Allows permittivity ratio up to 10 !

### Proposed techniques

A unified dielectric pre-characterization approach

- Experimental results with 3 TP-FPD structures
- □ Dielectric permittivity ranges from 1.0 to 7.0

| Case | RWC  | ap [13]      | Proposed method |        |       | Homogenization [9] |       |       |
|------|------|--------------|-----------------|--------|-------|--------------------|-------|-------|
|      | Time | Mem.         | Time            | Mem.   | Error | Time               | Mem.  | Error |
| 1    | 2.3s | 9.6MB        | 2.4s            | 12.4MB | <0.1% | 2.8s               | 251MB | <0.1% |
| 2    | 539s | 5.7MB        | 530s            | 11.2MB | <0.1% | 629s               | 250MB | <0.1% |
| 3    | 222s | 21 <b>MB</b> | 227s            | 34.7MB | 0.01% | 40.3s              | 273MB | -13%  |

- □ Homogenization approach with modification has large error
- □ The new approach is accurate and consumes less memory
- With only 177MB pre-characterization data, it suits to any dielectric profile of TP-FPD technology

### Proposed techniques

Parallel simulation on a computer cluster

- For accurately calculating the coupling capacitances, further acceleration is necessary
- Develop a parallel FRW algorithm for distributed computing



### Proposed techniques

- Parallel simulation on a computer cluster
  - Implemented with MPI on a homogenous cluster
  - $\Box$  Three test cases are run with 0.1% 1- $\sigma$  error



With 120 processes, the speedup is 91X, 111X and 113X

Notice in our previous work [GLSVLSI'2016], the speedup is at most 67X, under same settings

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### Conclusions

- Efficient resistance/capacitance calculation techniques have been developed for the design of high-quality FPD and TP-FPD
- The applications in Empyrean CAD toolset validated their effectiveness and practicality
- They have brought benefits to the time-to-market and yield of FPD products

# Thank You !



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